

Periglacial Geohazards at the Colne Valley South Embankment and Chiltern Tunnel Ventilation Shaft Design

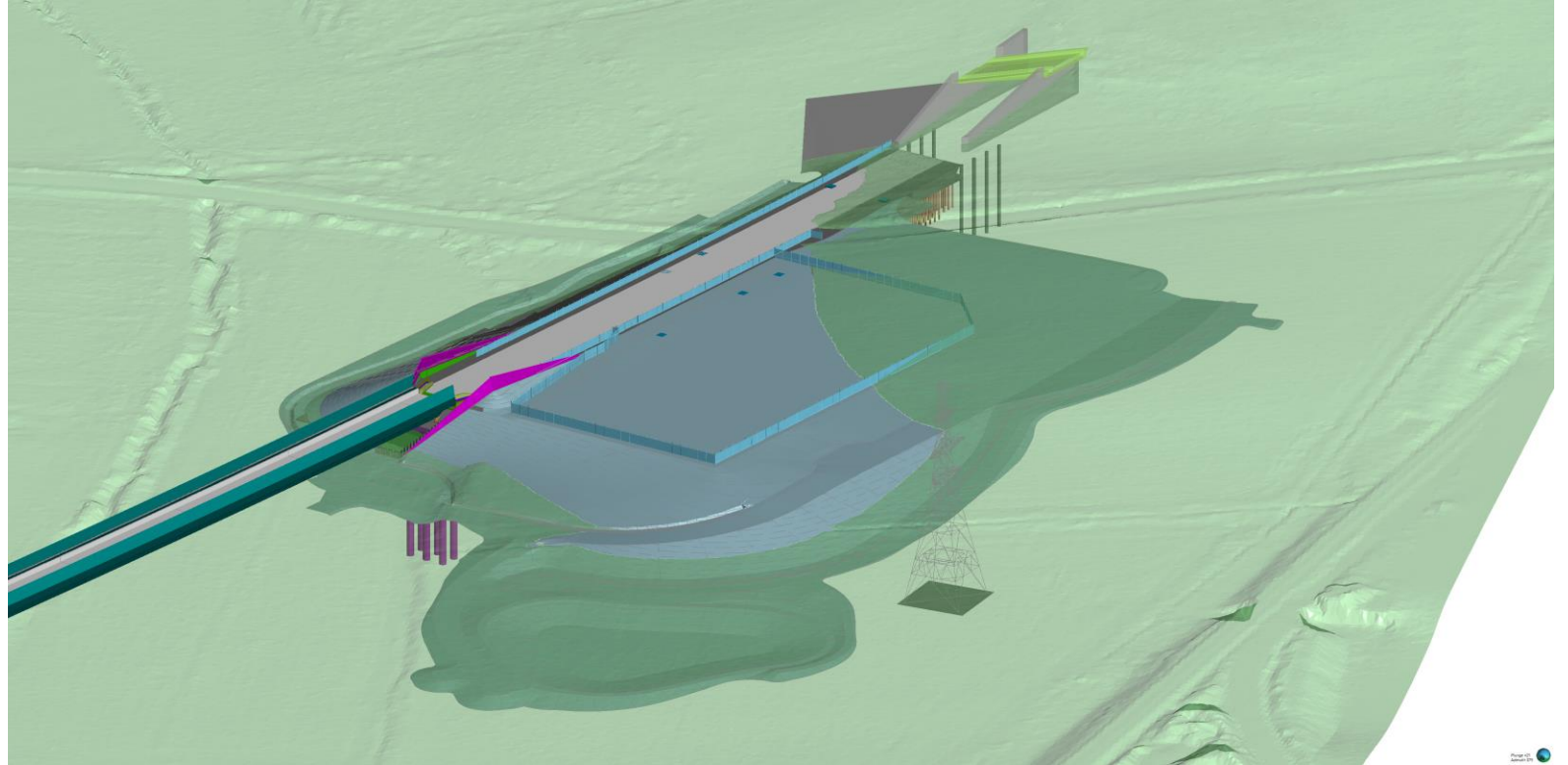
West Midlands Regional Group of The Geological Society

April 2024

Guillermo Mondejar (Jacobs)

Agenda

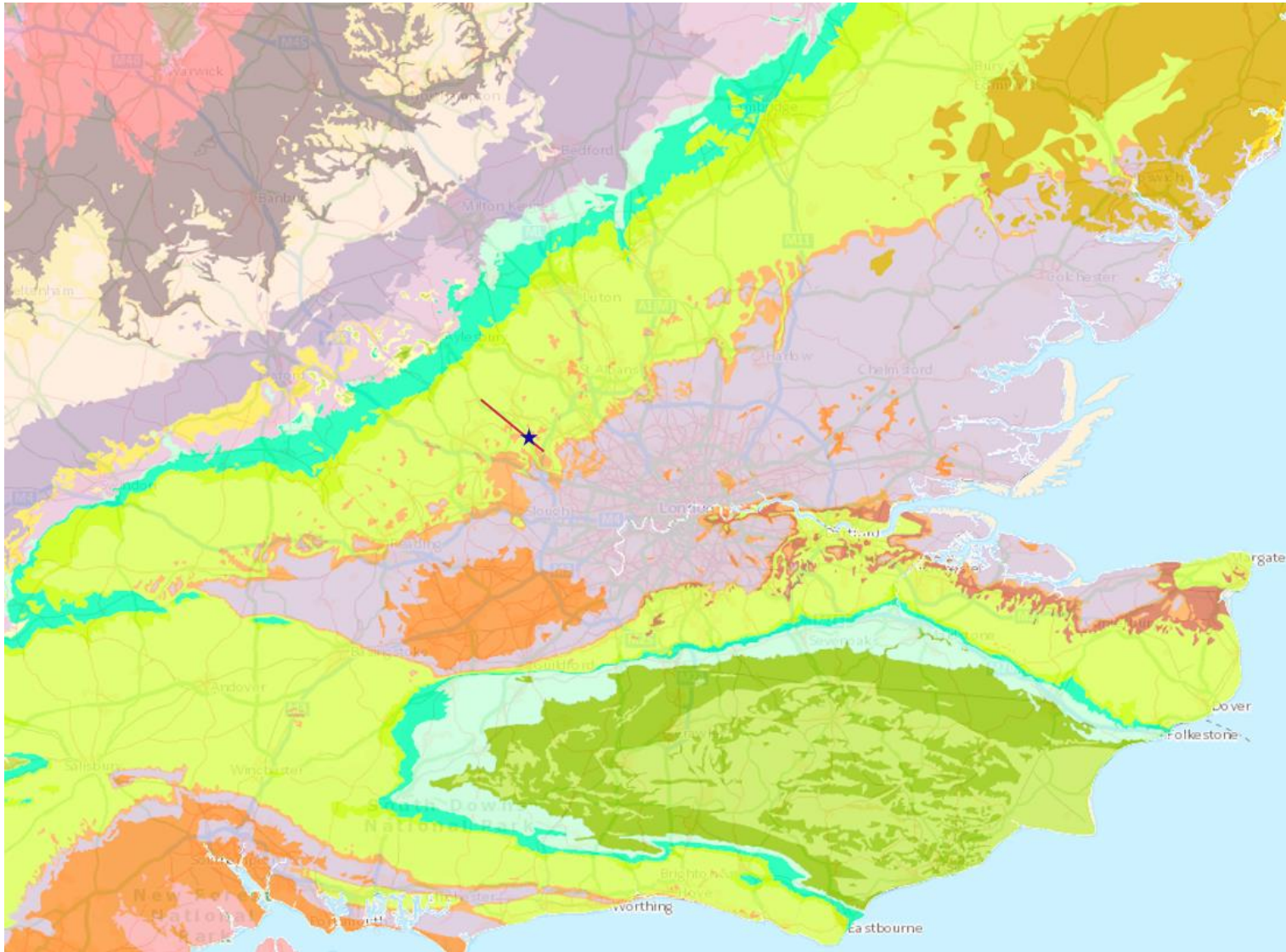
- Introduction to Contract C1
- Colne Valley South Embankment
 - Abstract
 - Site Location / Setting
 - Site Investigation and Testing
 - Geology and Ground Model
 - Relic Shear Surfaces
 - Design Evolution and Implications
 - Engineering Solution
- Chiltern Tunnel Ventilation Shafts
 - Ground Conditions
 - Geotechnical Design
 - Construction & Performance



C1 Works Overview

C1 Align – A Truly Integrated Project Team

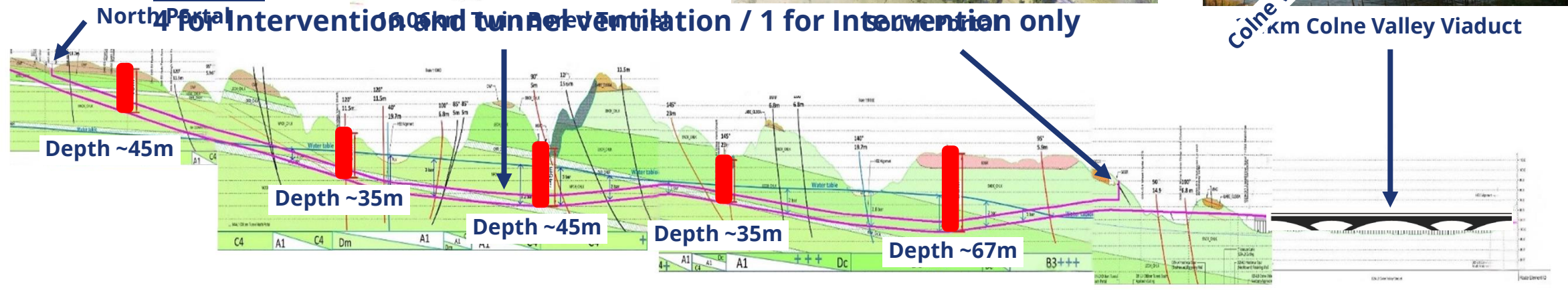
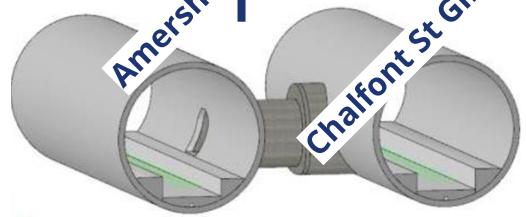
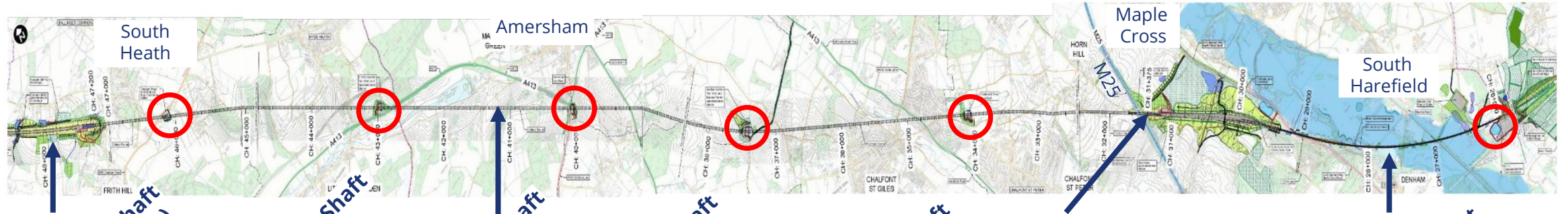




C1 Works Overview

- Colne Valley Viaduct, Earthworks and Tunnelling through the chalk geology of the Chiltern Hills
- The tunnel alignment cuts across the north limb of the London Basin geological syncline

C1 Works Overview



Periglacial Geohazards at the Colne Valley South Embankment

Abstract



Periglacial slip surfaces have different causes and mechanisms, but all present a potential geohazard to engineering works, in this case, embankment construction. Periglaciation can result in the presence of a mantle of material at or near the ground surface characterised by poor compressibility and strength characteristics, including the presence of shear surfaces with potential residual shear strength values. There are significant periglacial shear surfaces recorded in the Denham area (particularly associated with the construction of the M25). The most well-publicised are solifluction shears recorded in the London Clay.



During the interpretation of the ground investigation, and subsequent ground modelling for the detailed design of the High Speed 2 Colne Valley South Embankment, Jacobs confirmed the presence of periglacial Head Deposits and relic shear surfaces occurring within the Head Deposits and underlying Reading Formation (Lambeth Group). Test data demonstrated poor engineering characteristics including residual strength values lower than those assumed during the 'preliminary' and 'scheme' design phases which required reconsideration for the detailed design and construction proposals

Site Location / Setting

Site Location / Setting

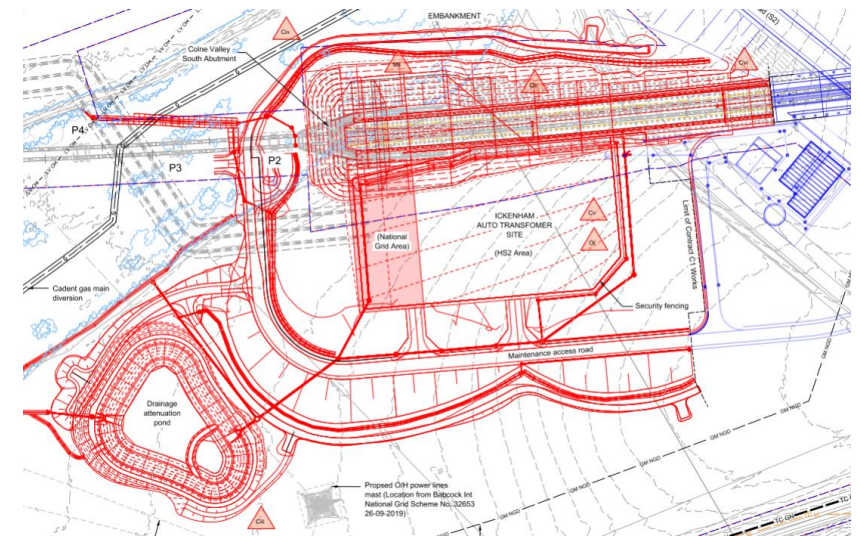
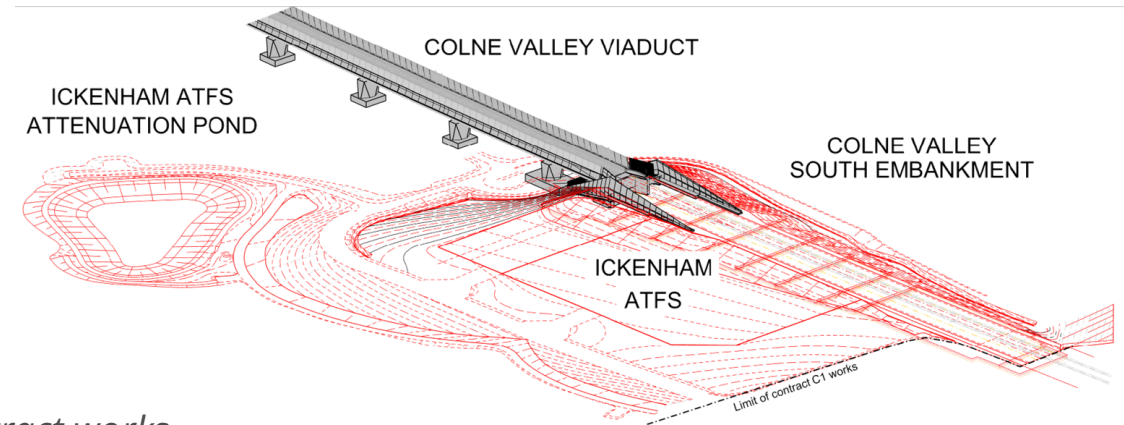
Colne Valley South Embankment (CVSE):

- Southern approach to the Colne Valley Viaduct to the North
- Transitions into Copthall Tunnel portal to the south (S2 Contract)
- HS2 Chainage from 025+810 to 026+010
- 200m long
- 10m high

Requires the permanent diversion of Harvill Road. as part of separate S2 contract works which also include the construction of the Copthall Tunnel portal and Copthall Tunnel portal building, located east of the Ickenham ATFS.

Ickenham Auto-Transformer Feeder Station (ATFS)

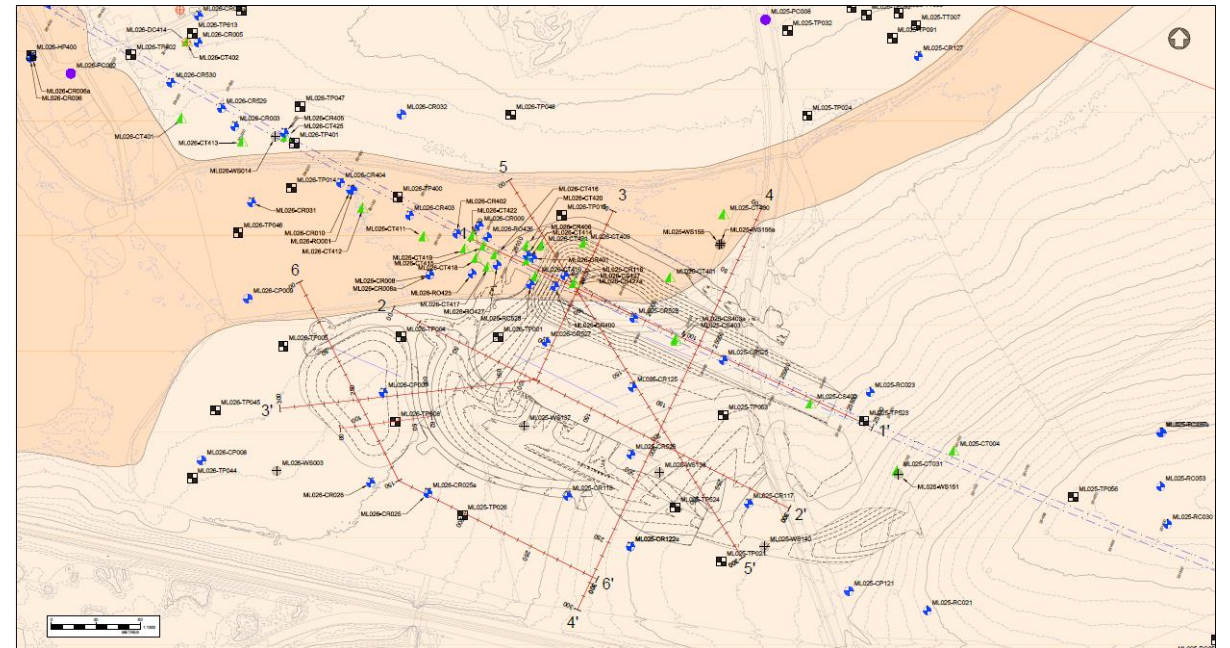
- Earthworks platform south of the CVSE between approximate Ch. 025+885 and Ch. 026+010.
- 125m x 65m (level with the CVSE).
- Includes the construction of a drainage attenuation pond permanent maintenance access roads / tracks serving the Ickenham ATFS, CVSE and CVV.



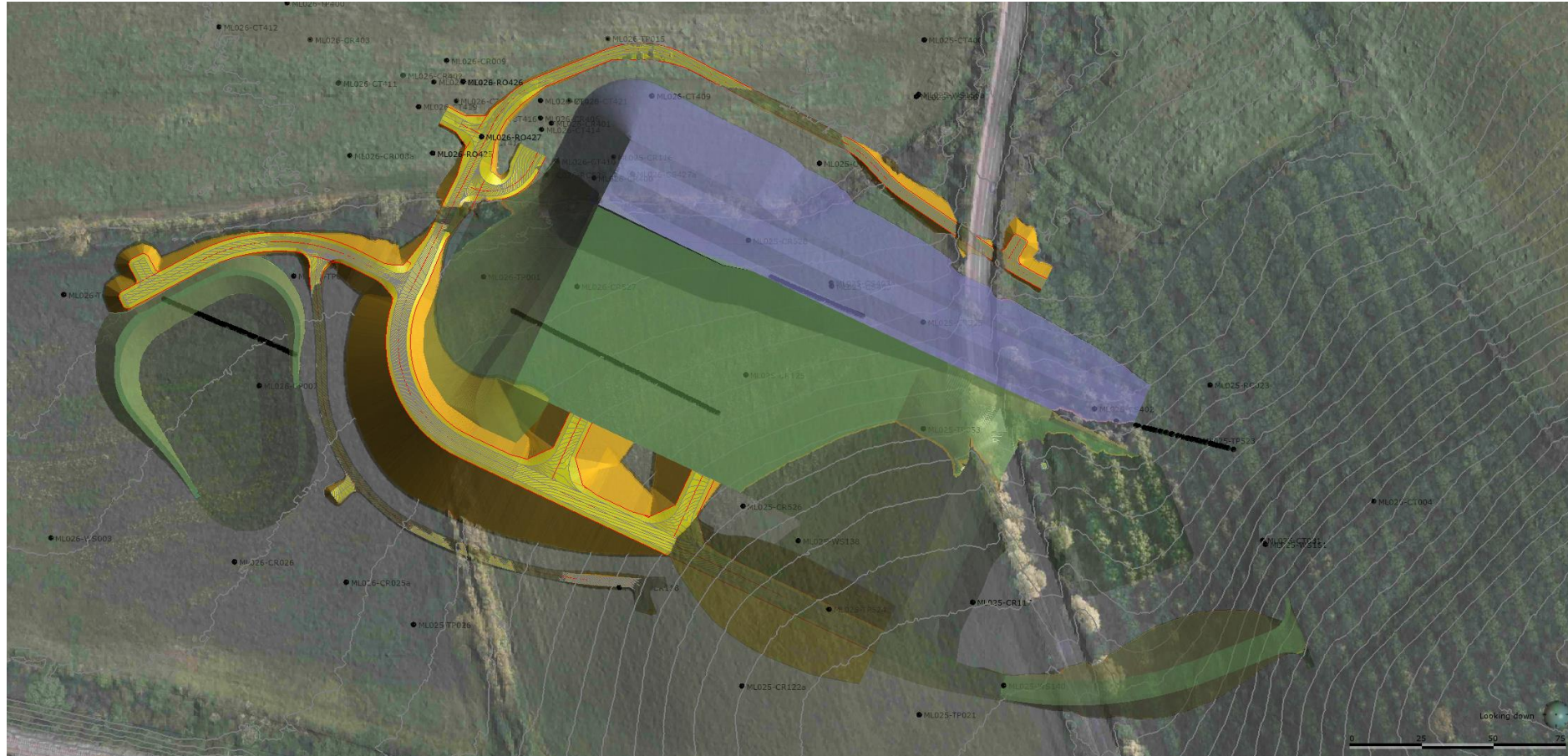
Site Investigation and Testing

Site Investigation and Testing

1. HS2 Main GI in this area was limited by protester activities, resulted in limited preliminary GI
2. Supplementary C1 GI Phase 1 limited by protester activity, archaeology, and viaduct compound area
3. **Supplementary C1 GI Phase 5 Boreholes and Trial pits completed summer 2020**
 - Laboratory testing
 - 254 Laboratory Test Completed
 - Surface MASW Geophysics undertaken in September 2020
 - RSK (1 Geophysical Surveys)
 - Zetica (3 Geophysical Surveys)



Site Investigation and Testing



Geology and Ground Model

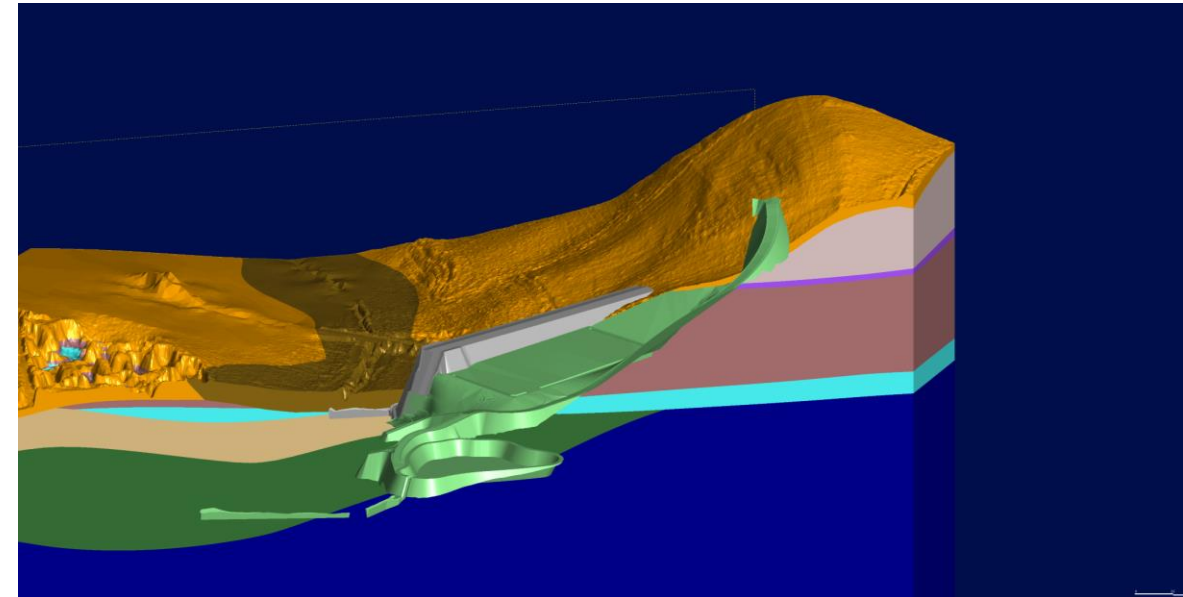
Geology and Ground Model

Superficial Deposits:

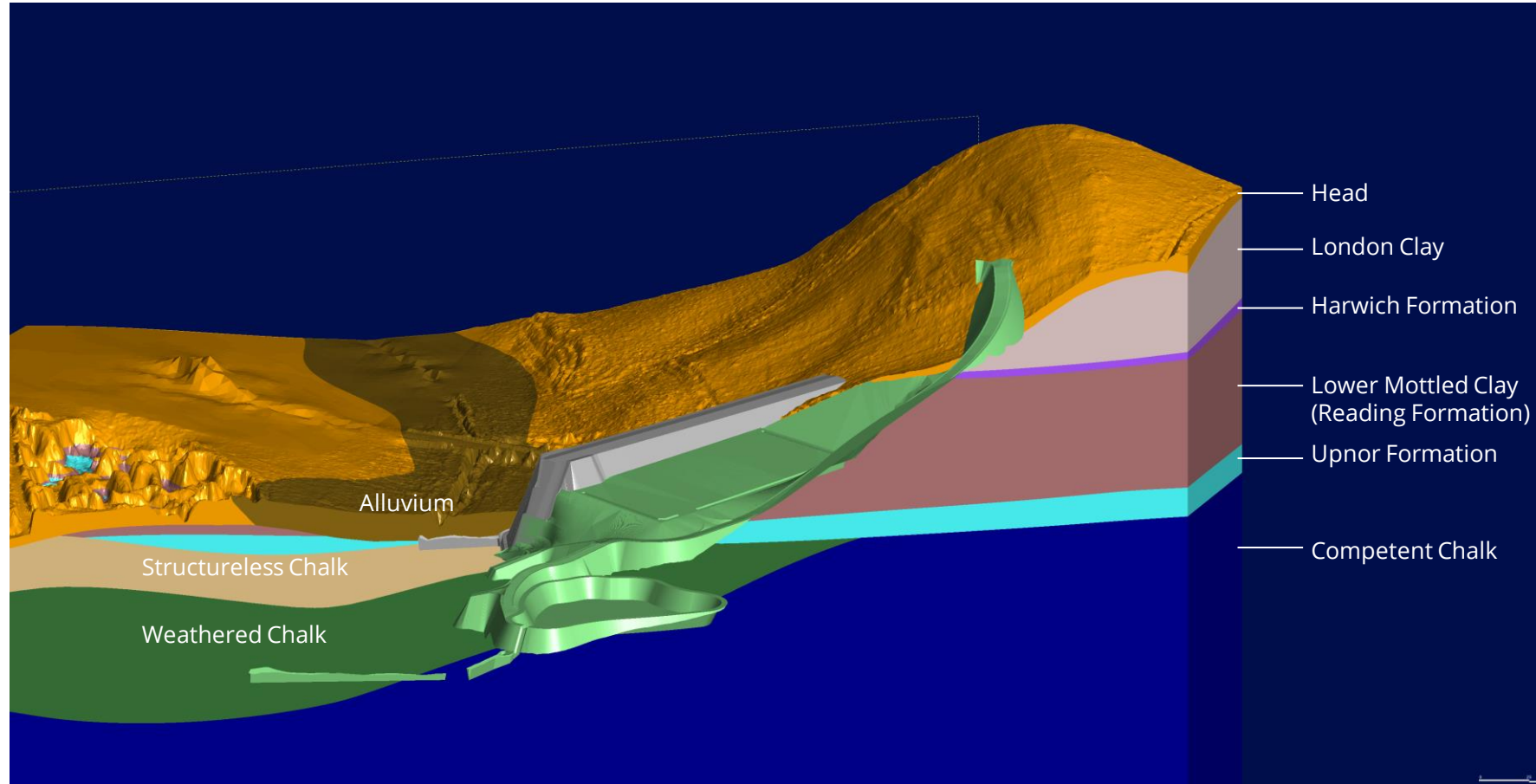
- Alluvium (ALV) at the viaduct southern abutment and across the valley floor
- Head forming a blanket over the slope

Solid Geology

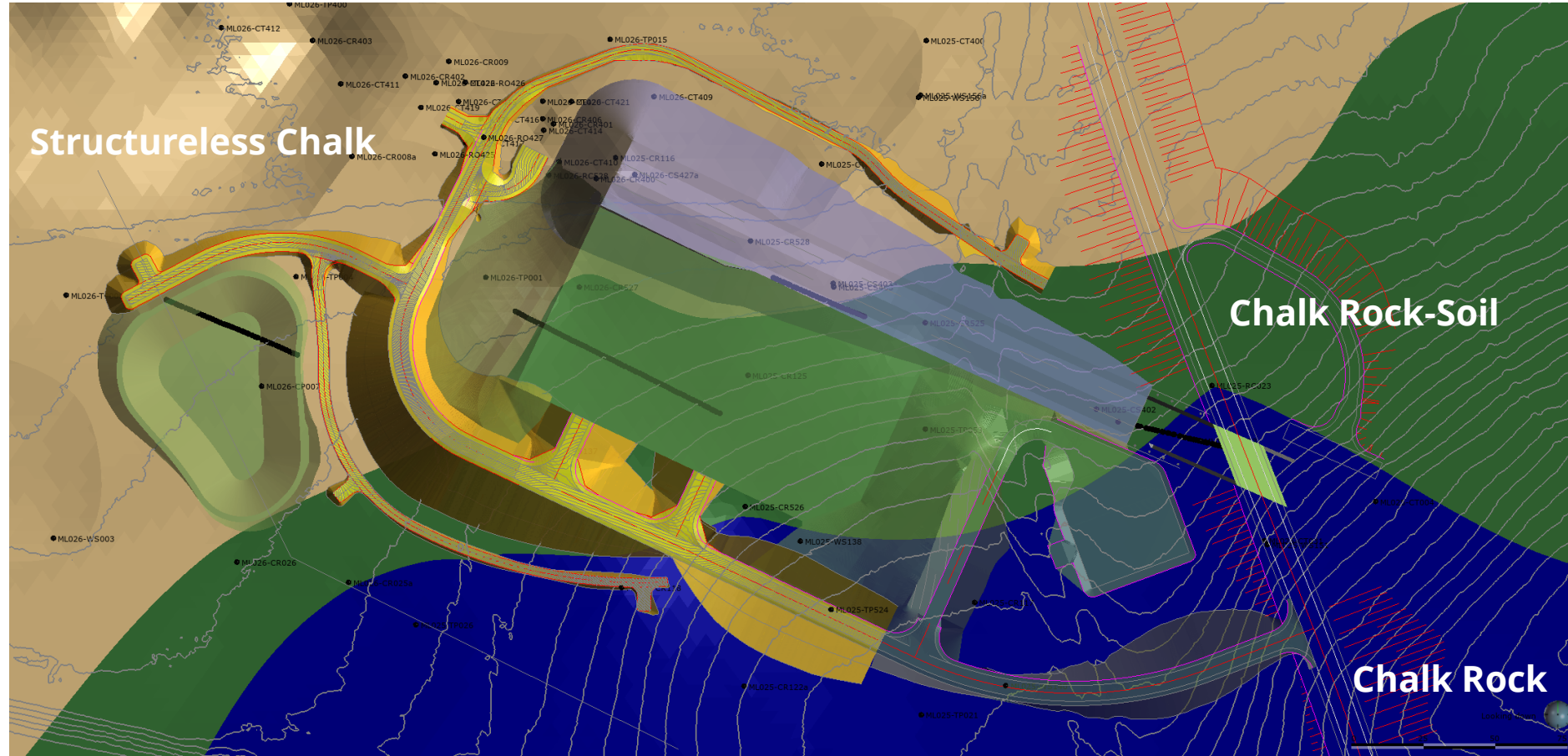
- London Clay (LC) forms the upper part of the hill,
- Harwich Formation (HWH) is a thin relatively granular layer
- Reading Formation - Lower Mottled Clay (LMCL)
- Upnor Formation (UPR), thin layer of sand and clay,
- Upper Chalk weathering sequence underlying the valley floor:
 - Structureless chalk
 - Weathered chalk
 - Competent chalk



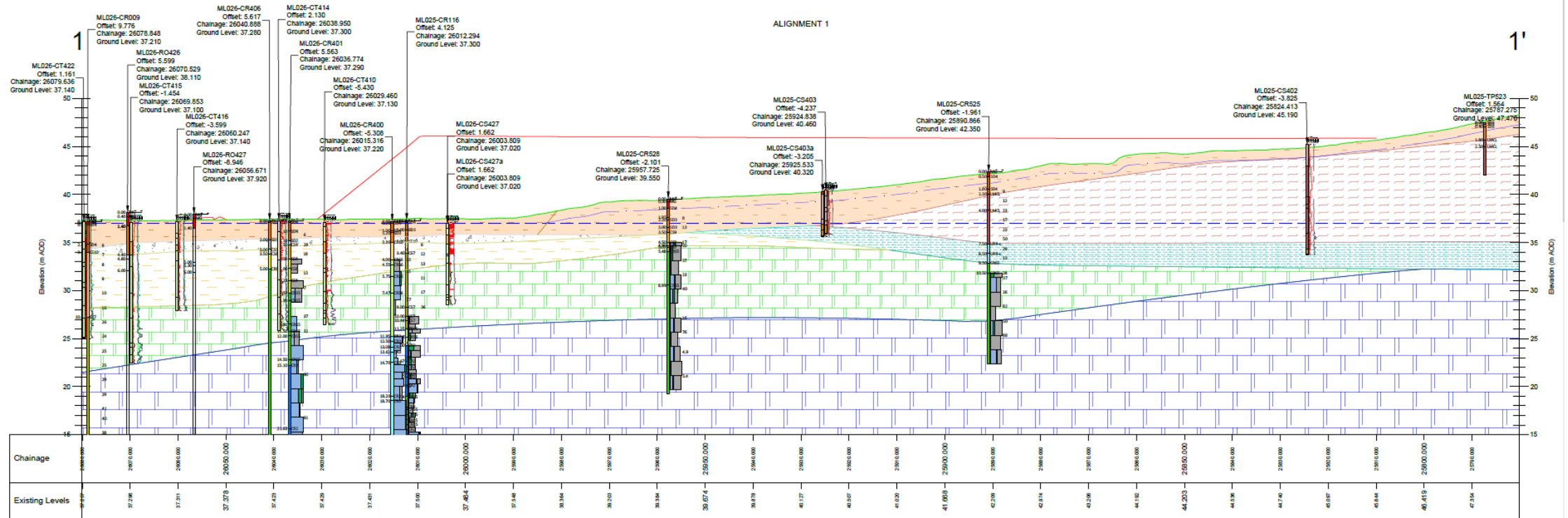
Geology and Ground Model



Geology and Ground Model



Geology and Ground Model



Profile Legend:

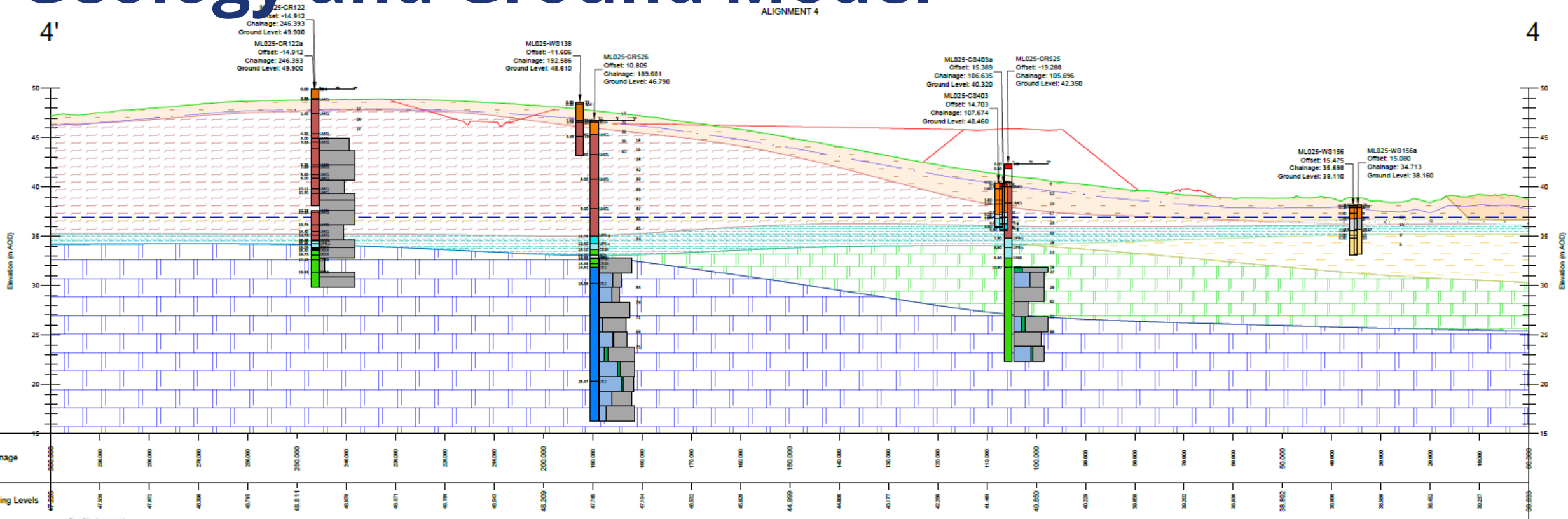
- Superficial deposits Alluvium (SD4)
- Superficial deposits Head (SD3 / SD4)
- Superficial deposits granular (SD1 / SD2)
- London Clay
- Harwich Formation
- Reading Formation (Lower Mottled Clay)
- Upnor Formation (UPR-c / UPR-g)
- Structureless Chalk Grade Dm (CS9 / CS10)
- Weathered Chalk (CRS - Treat as CRS5 / CRS6)
- Competent Chalk (CR - Treat as CR2)

Geology and Ground Model

ALIGNMENT 4

4'

4



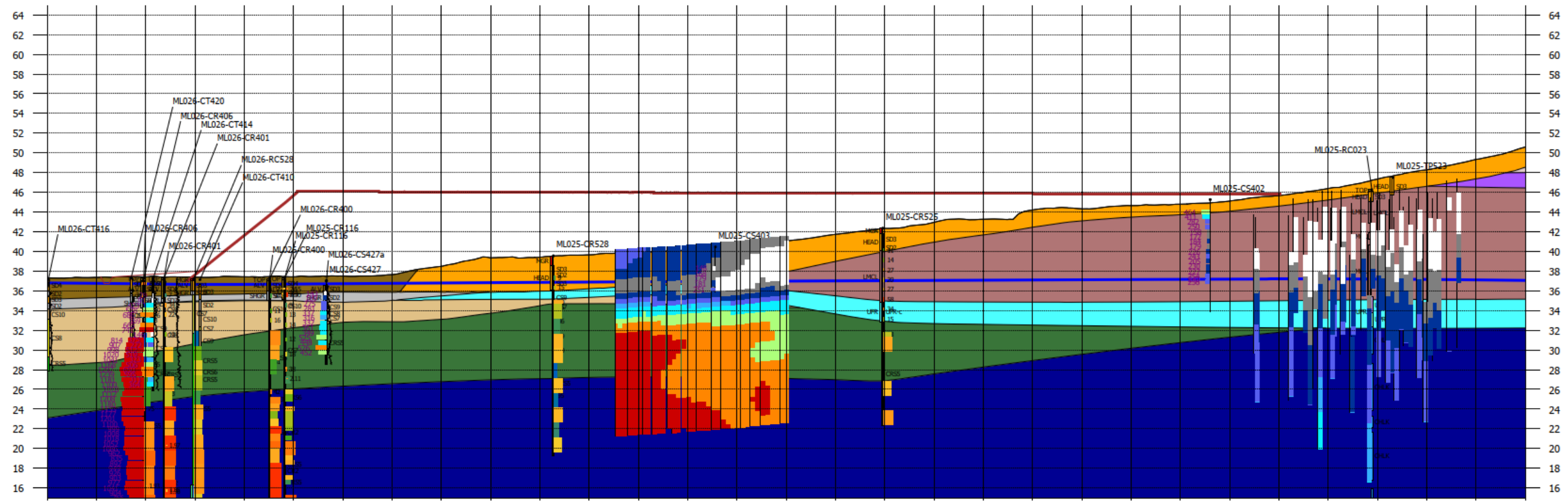
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Geology and Ground Model

A

B



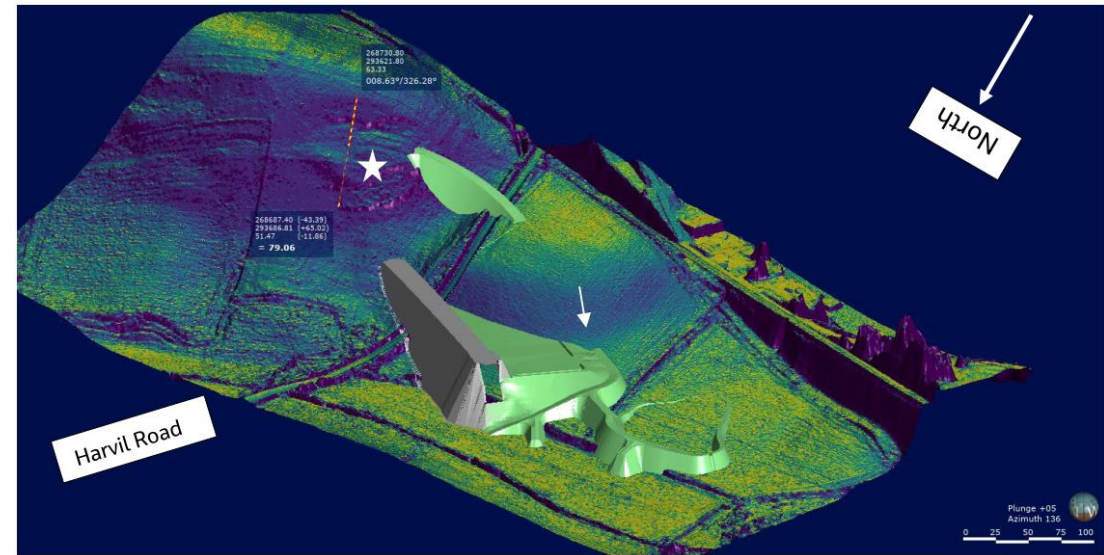
Legend

Geology_Code			Engineering_Grade			SCR	N60	MASW (Min Vs)			Downhole/SCPT							
ALV	LECH	PEAT	TOP	CHLK	CRS6	FLNT	SD4	0	25	50	75	100	≤ 150	≤ 300	≤ 570	≤ 150	≤ 300	≤ 570
HEAD	LMCL	SFI	UPR	CR1	CS10	PEAT	UPR-c	1	16	31	45	60	≤ 180	≤ 330	≤ 690	≤ 180	≤ 330	≤ 690
HWH	MGR	SHGR		CR2	CS7	SD1	UPR-g						≤ 230	≤ 450	> 690	≤ 230	≤ 450	> 690
LC	OH	SU		CR3	CS8	SD2												
				CRSS	CS9	SD3												

Relic Shear Surfaces

Relic Shear Surfaces

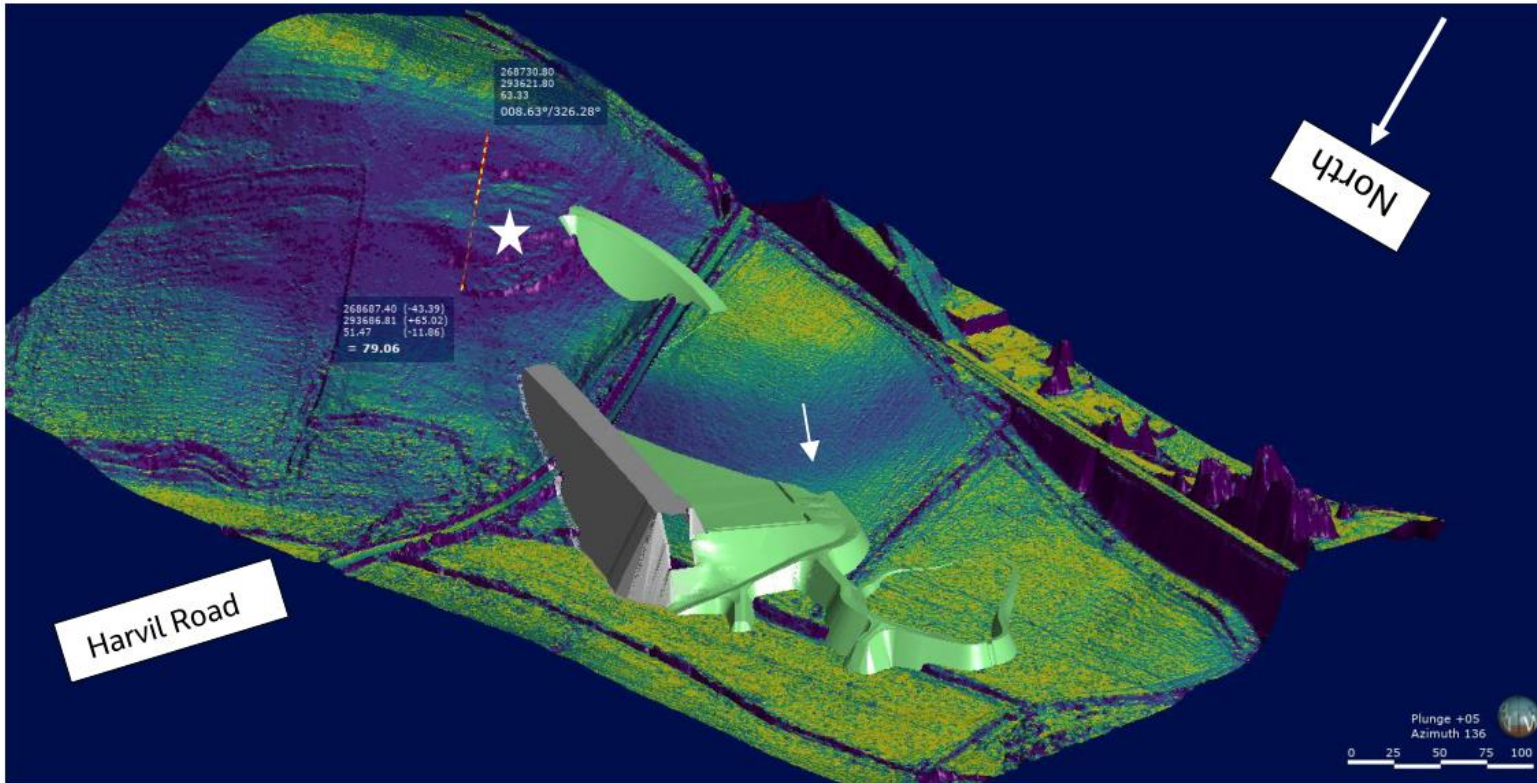
- Detailed interpretation of the available LiDAR topographical surface allowed to reveal relic landslips within the site area
- Features were found on a natural hillside slope of around 9 degrees from horizontal
- The gradient of the slope to be considered stable was only 5 degrees.
- The sub-surface ground model clearly showed the depth of Head deposits gradually increasing towards the toe of the slope, suggesting significant downslope movement during periglacial climatic conditions of the Late Pleistocene.)



5x Vertical Scale

Relic Shear Surfaces

Polished slip surface at 2.0m depth, showing the morphology of the slip surfaces



5x Vertical Scale



Relict Landslip feature identified at 4.5 to 5.0m depth



Relic Shear Surfaces

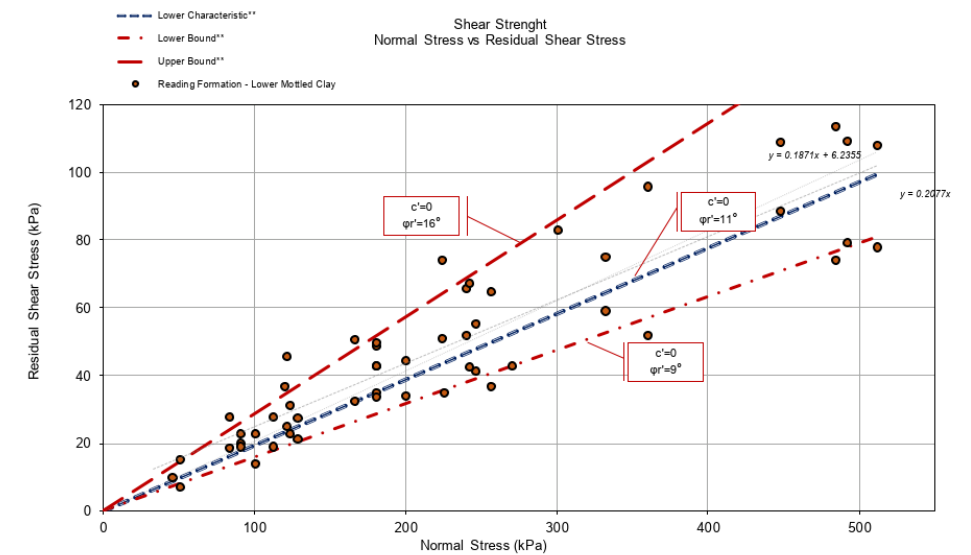
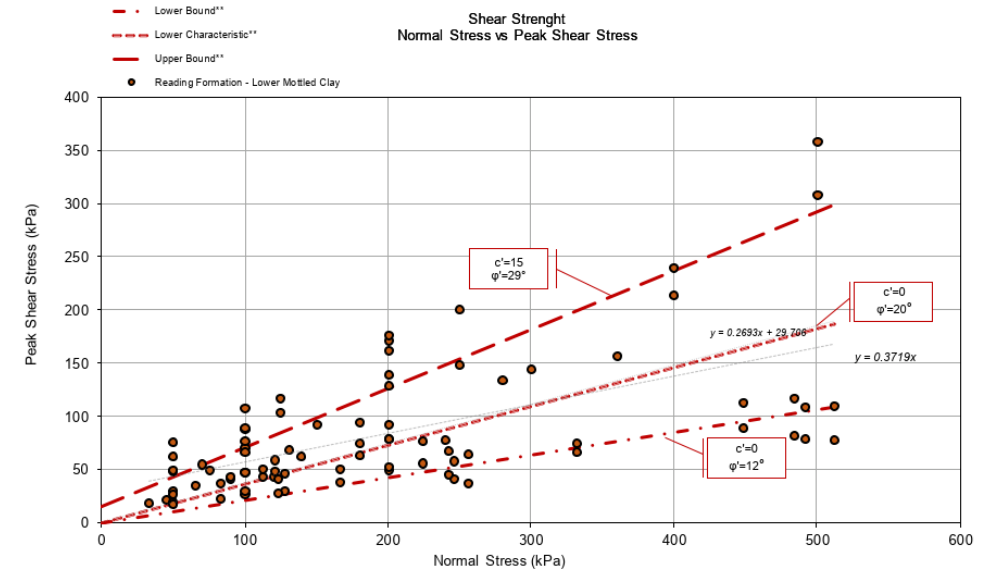
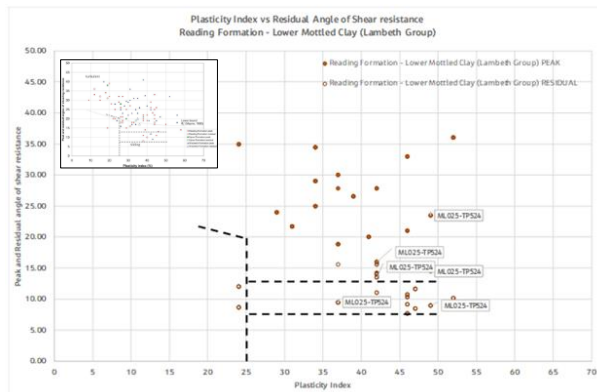
It was concluded that the data validated design values to be set based on lower characteristic values compared to preliminary design.

GL to 8m depth design on residual shear strength properties:

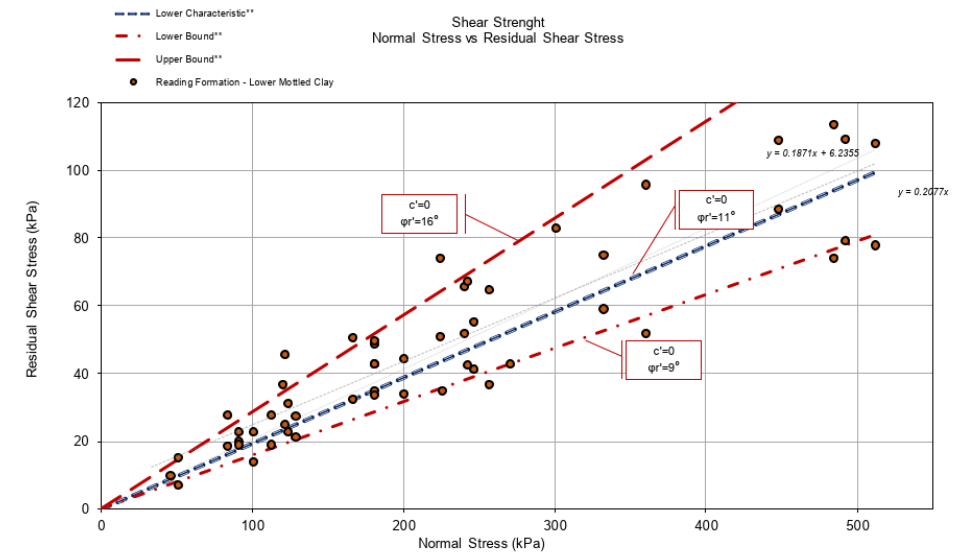
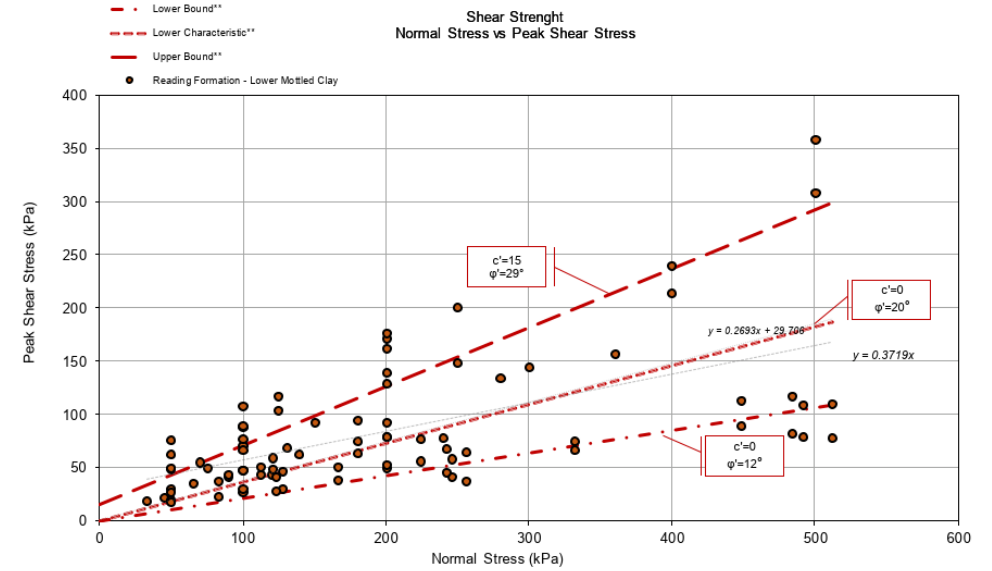
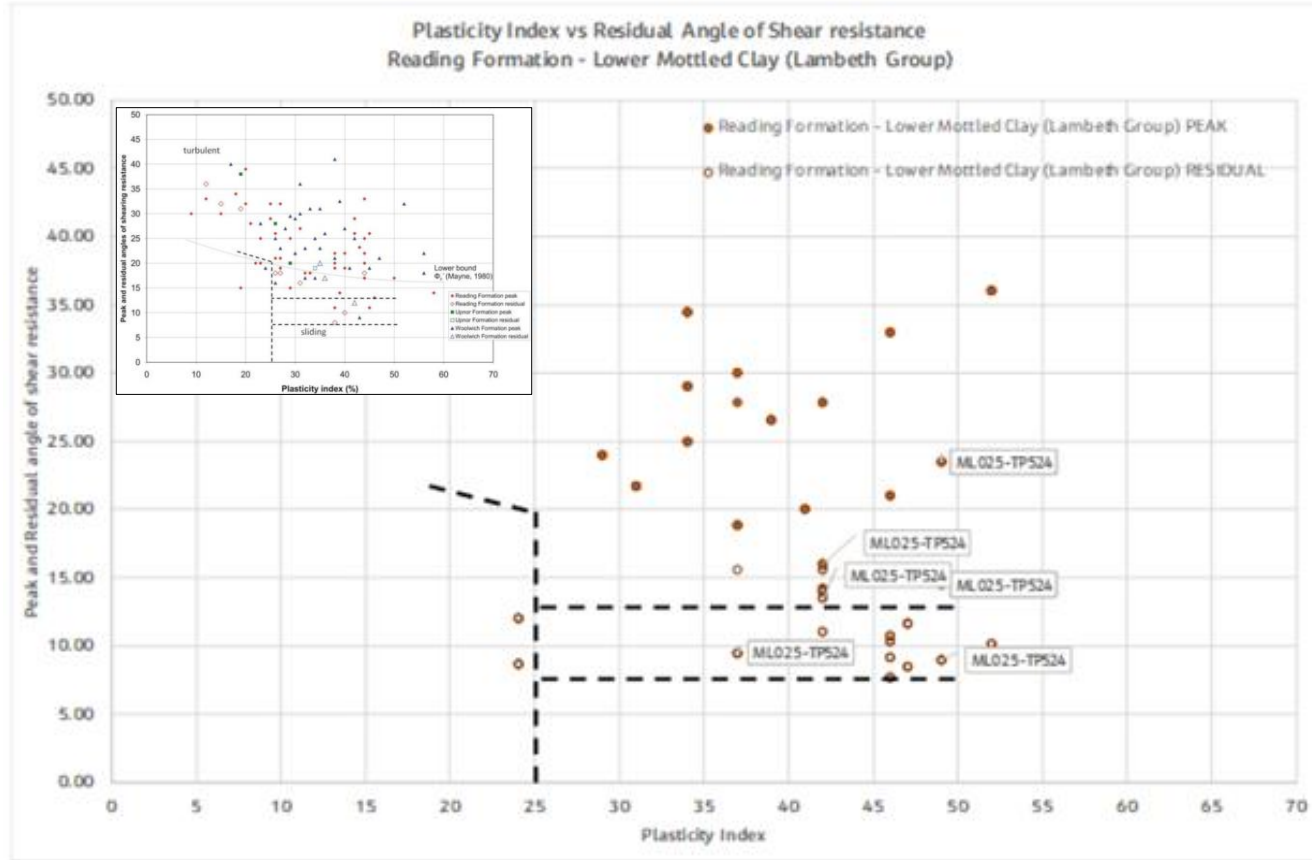
- $C'_r = 0\text{kPa}$
- $\Phi'_r = 11\text{ degrees}$

>8m depth design on peak shear strength properties:

- $C'_p = 0\text{kPa}$
- $\Phi'_p = 20\text{ degrees}$



Relic Shear Surfaces



The BGS report Engineering Geology of British Rocks and Soils - Lambeth Group (Open Report OR/13/006) reviews both triaxial test results and shear box data for the various strata of the Lambeth Group including the Reading Formation that includes the Lower Mottled Clay. It comments that "Only a few residual shear strength values were available"

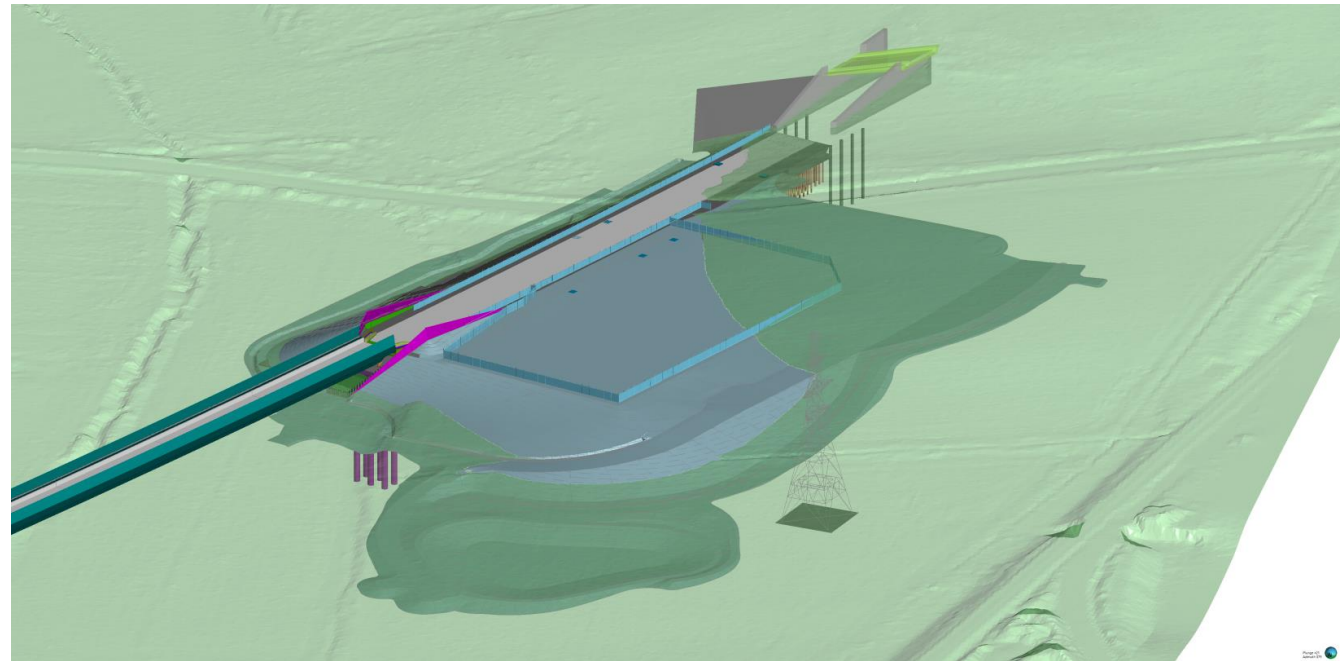
Design Evolution and Implications

Design Evolution and Implications

1. Preliminary design assumed slope stability relying on residual strength for the superficial deposits and Lambeth group considering relict slip surfaces were likely to be present
2. ϕ'_r was set at a typical average value of 16 degrees, with limited testing and data to confirm this assumption
3. Subsequent laboratory test data demonstrated a lower ϕ'_r value of 11 degrees was appropriate (a reduction of 31%).

Implications on the scheme:

- **Increase in Foundation Treatment by extending length and distribution of driven piles including piles under the west shoulder of CVSE**
- **Lower embankment fill to be formed of cement stabilised chalk**
- **Extensive Geotechnical Instrumentation**



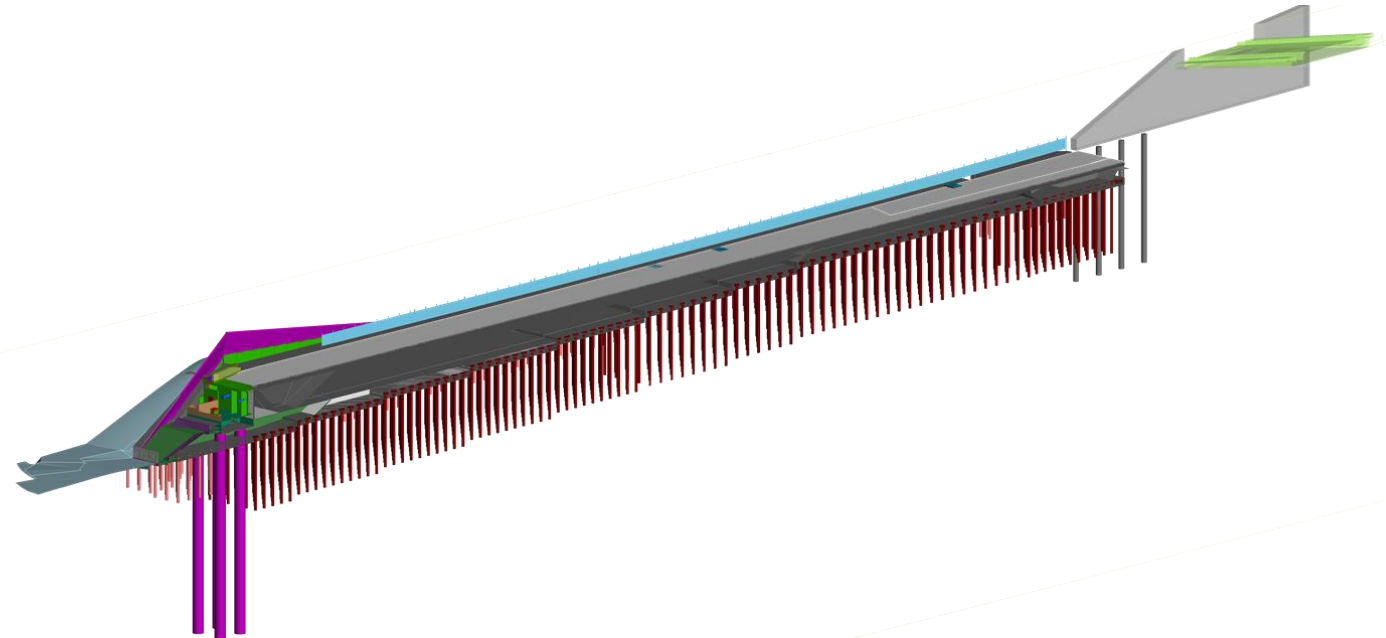
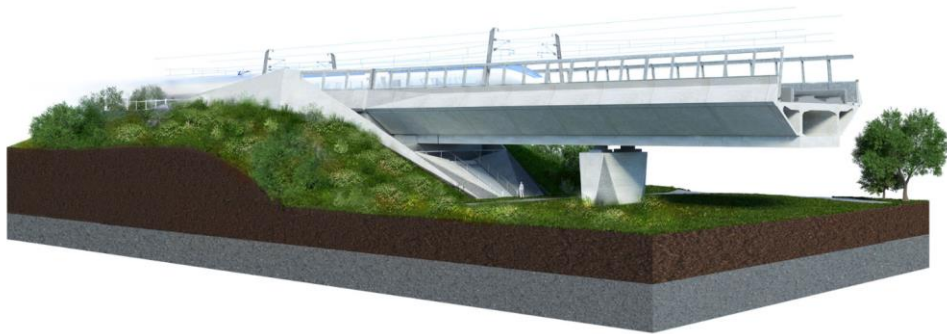
Engineering Solution

Engineering Solution

To mitigate the risk of excessive total / differential settlement and also instability associated the potential presence of relic shear surfaces, the CVSE is supported on piled foundation.

The piles along the CVSE fall into two categories:

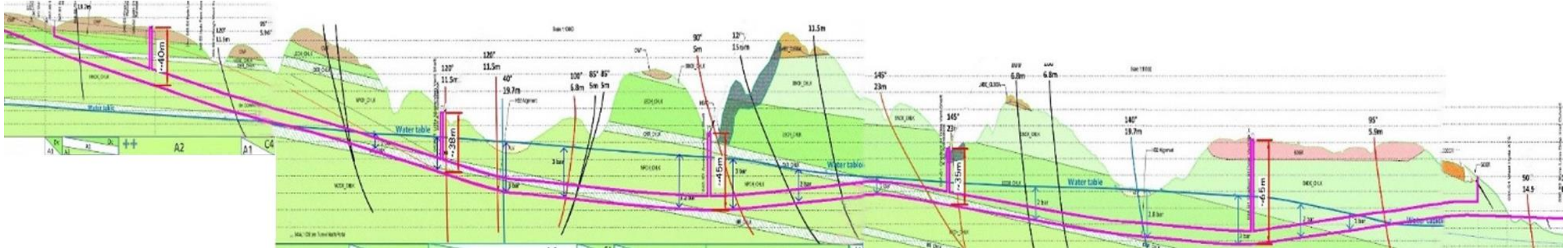
- Settlement reducing piles: Piles located beneath the embankment that carry the permanent and variable actions.
- Slope stabilising piles: Piles located beneath the edges of the embankment slopes to increase overall stability and vertical loads associated with the embankment shoulders.



Chiltern Tunnel Ventilation Shaft Design

Geological Setting

Geological Setting



Desk Study Long Section

- Shafts located to limit the amount of excavation
- Typically located in chalk dry valleys with variable thickness of Clay-with-Flints and high presence of dissolution features within the Chalk
- Example from Chalfont St Giles – Junction of 3 dry valleys



Geological Setting at Chalfont St Giles



Ground Investigation

Ground Investigation

Ground Investigation in chalk is complicated by chalk weathering and tendency to breakup during drilling. Shaft design required clear identification of chalk condition:

- Completely weathered chalk soil
- Weathered chalk with some structure but open / infilled joints
- Competent chalk with closed fissures
- Geological fault zones & dissolution features



Chalfont St Giles – Televueer looking horizontally

Ground Investigation

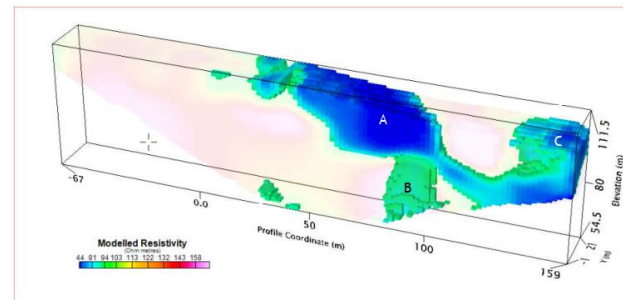
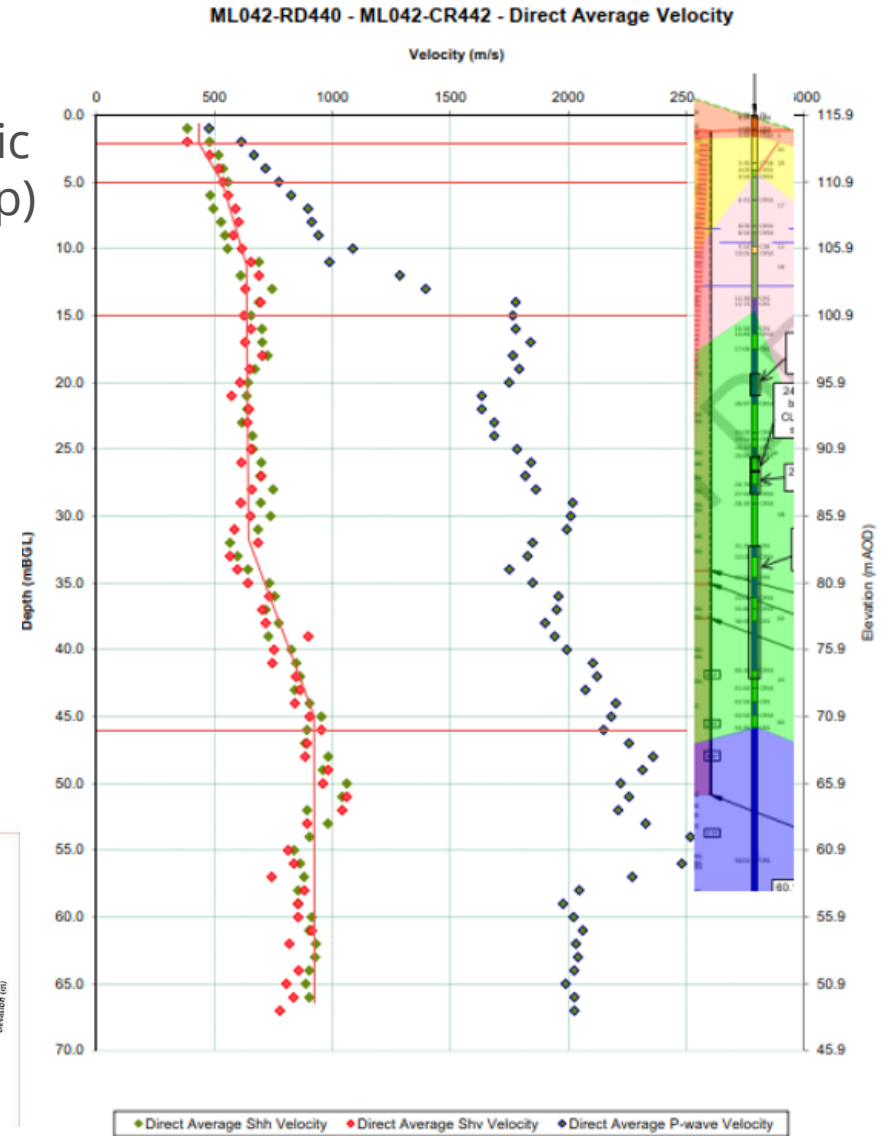


Chalfont St Giles



HPD

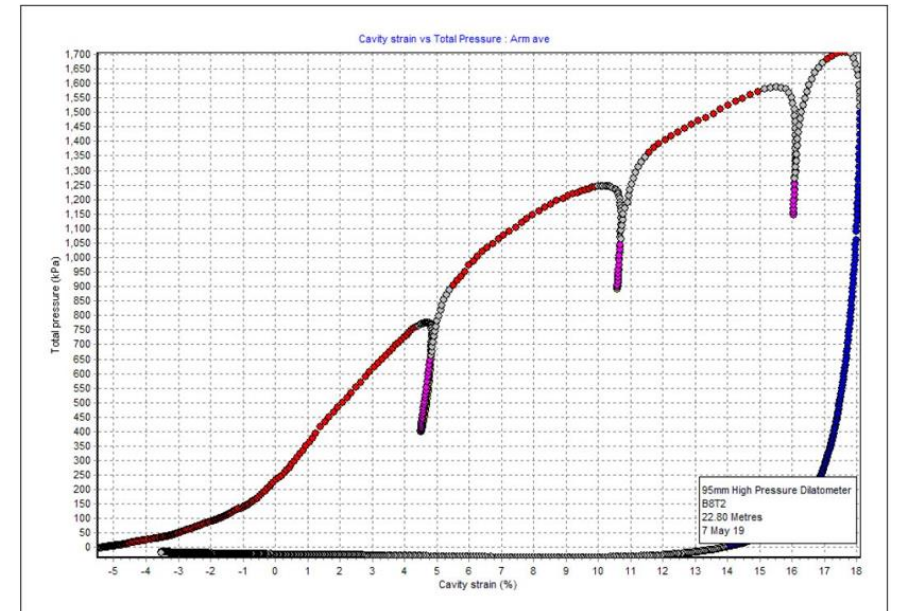
Cross-hole seismic geophysics (V_s , V_p)



3D Resistivity

Soil properties for design

- Pumping well tests: mass permeability (before & after D-wall)
- Pressuremeter testing: Es50 & horizontal earth pressure for K_0
- Cross-hole geophysics: small strain stiffness



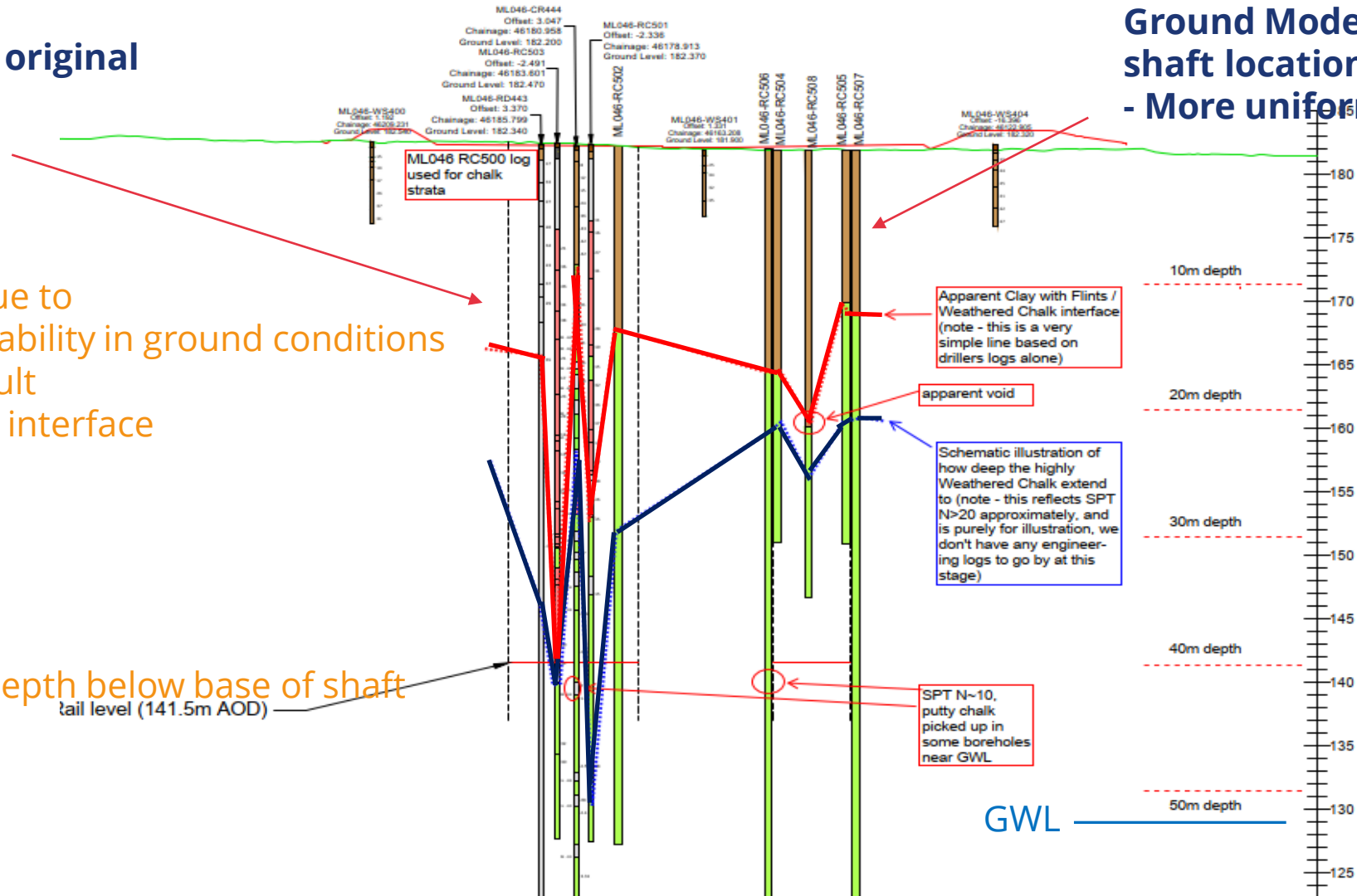
Ground conditions at Chesham

Ground Model at original shaft location
- More variation

- Shaft relocated due to
- significant variability in ground conditions
 - Presence of fault
 - Depth of chalk interface

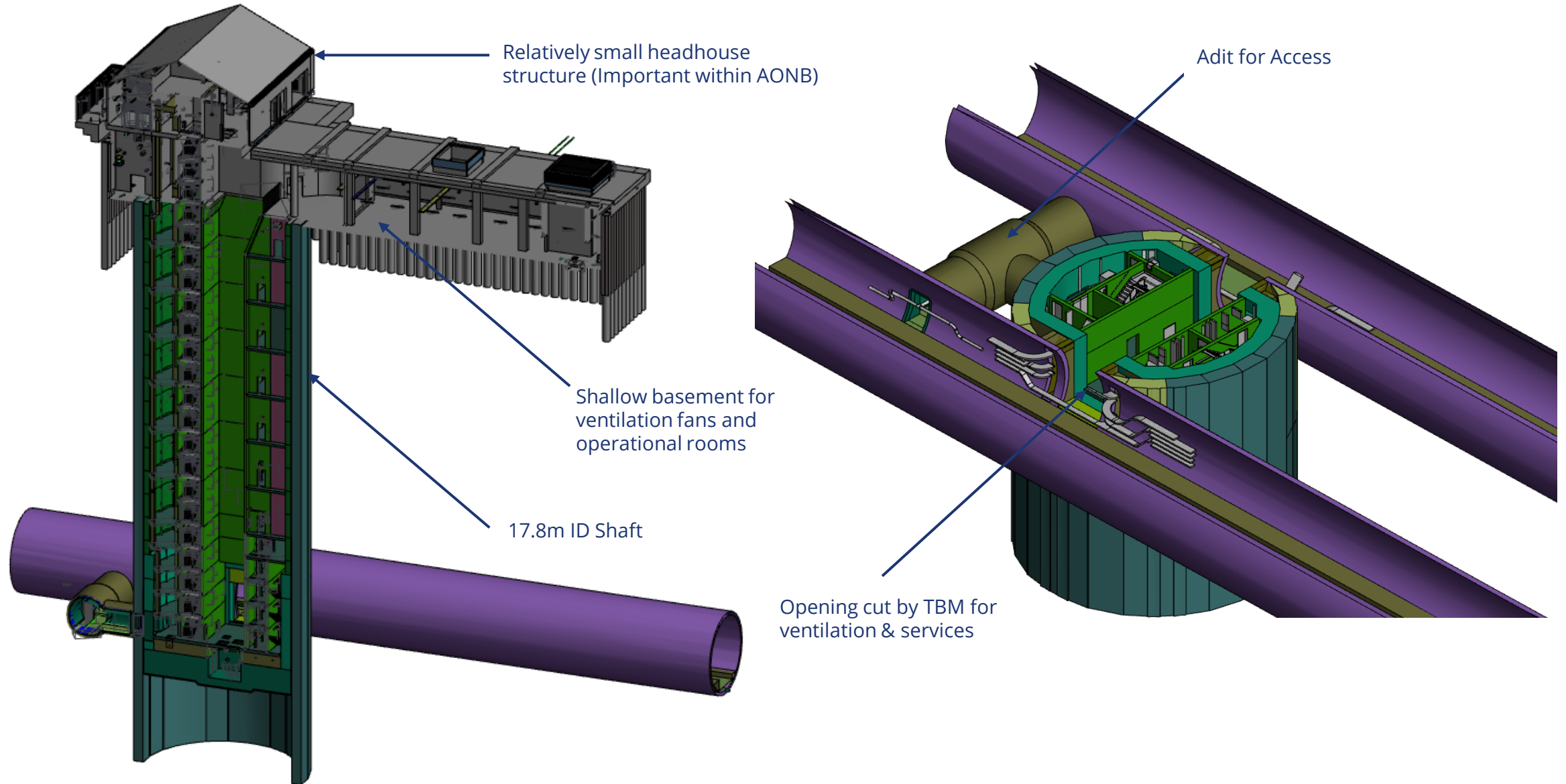
Groundwater at depth below base of shaft
tail level (141.5m AOD)

Ground Model at new shaft location
- More uniform



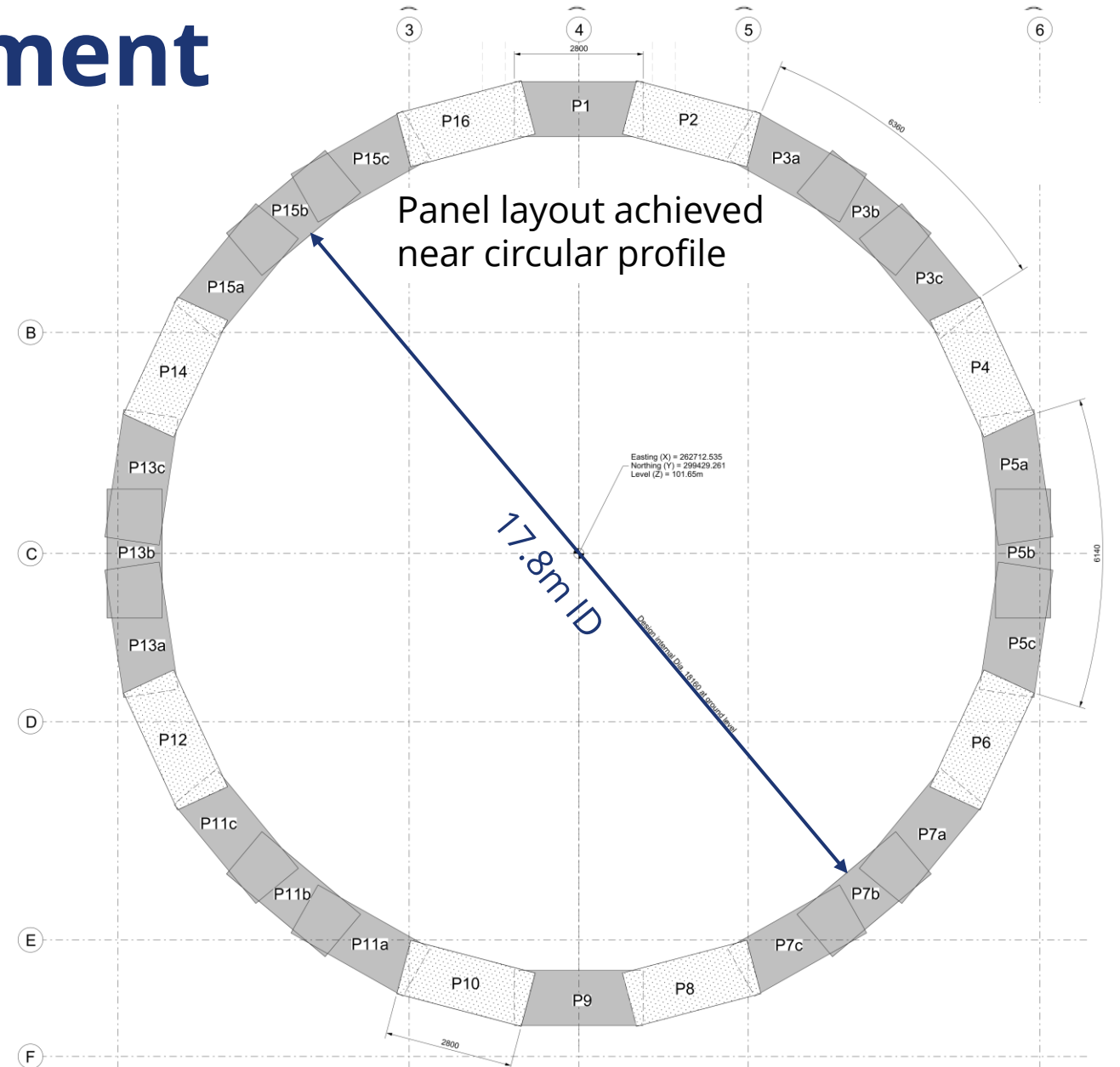
Design Solution

New / Innovative Design Solution



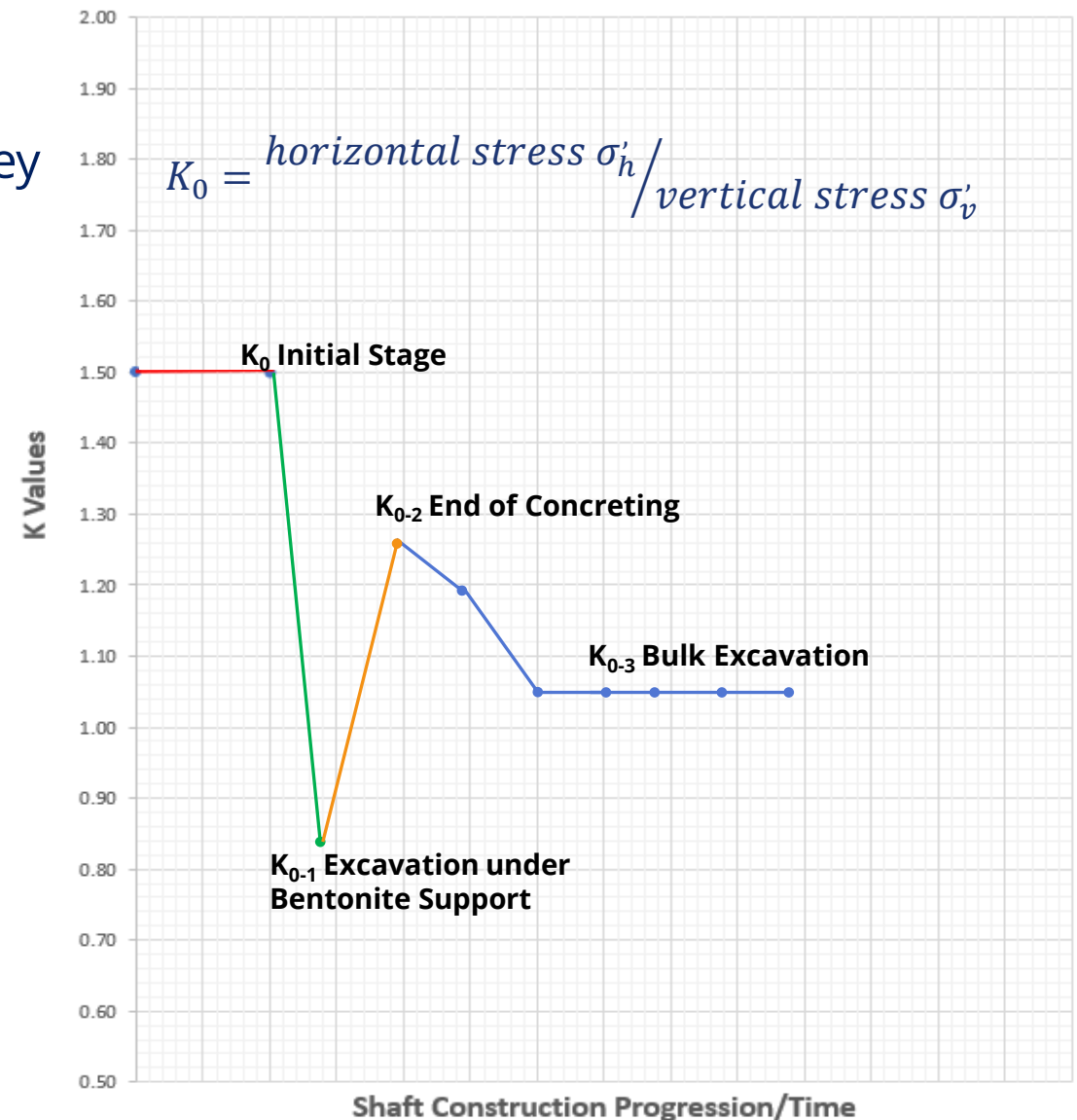
CSP D-Wall Arrangement

- Design developed in collaboration with KVJV
- Diaphragm Wall Depth: 78m
- D-wall thickness: 1.2m
- Construction tolerance 1 in 400 vertical plus 25mm positional
- I&M comprised:
 - Inclinometers within D-Walls
 - Surface monitoring points ●
 - Vibrating wire strain gauges ◆
 - Vibrating wire Piezo-meters ●
 - Trigger values determined by design



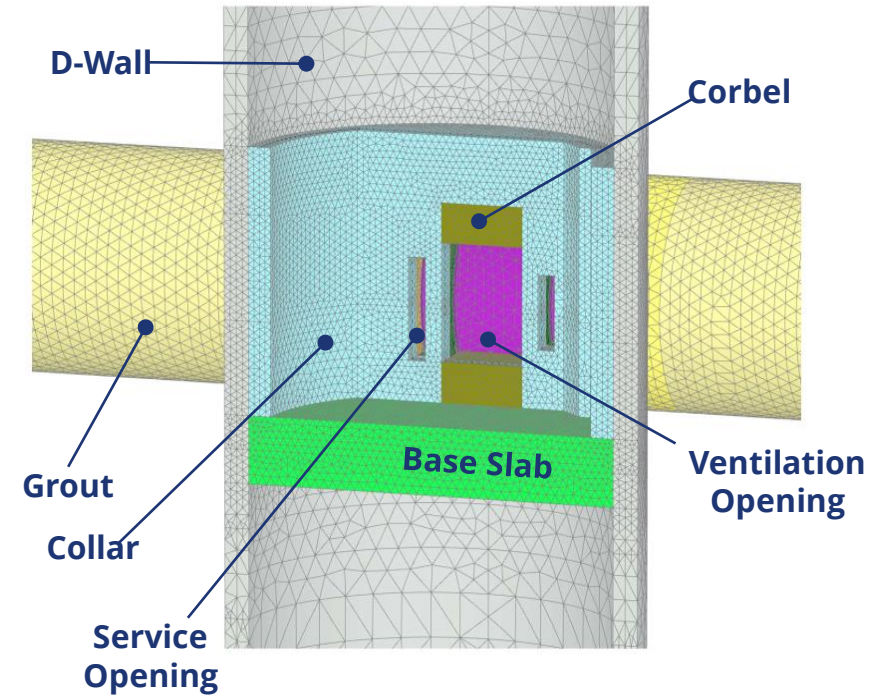
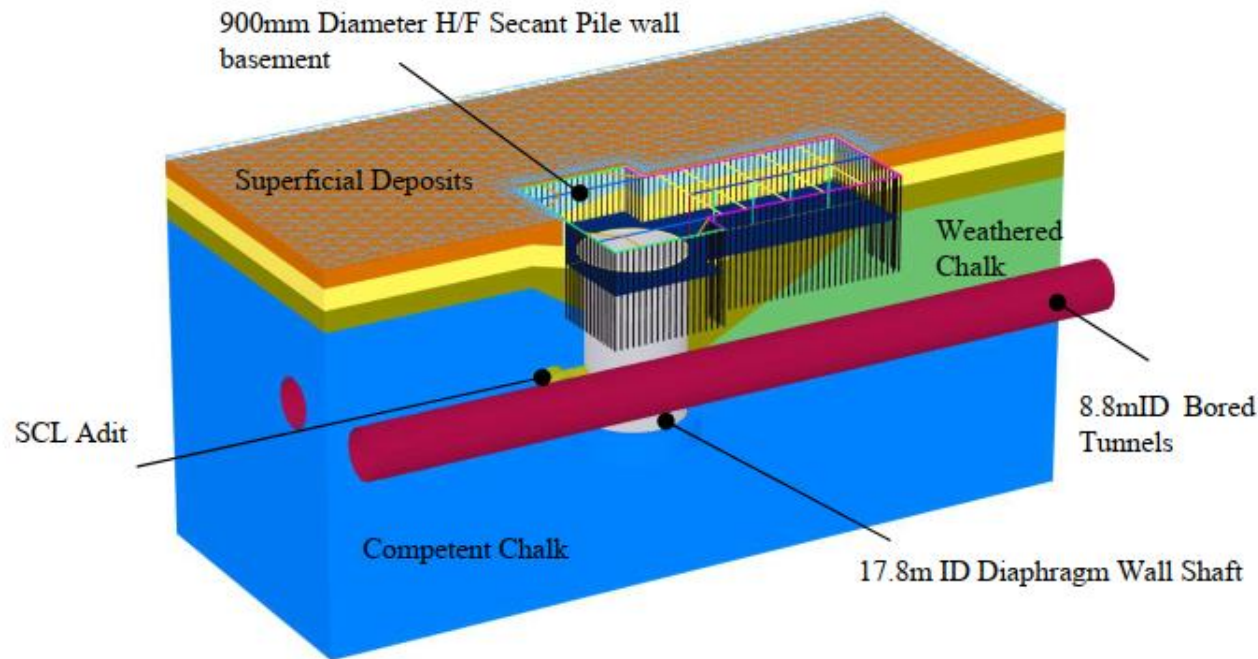
Design Consideration

- Lateral Earth Pressure Coefficient at rest $K_0 = \sigma'_h / \sigma'_v$ a key parameter for shaft design
 - Initial value (pre-construction) from insitu testing
 - Lateral earth pressure coefficient, K changes during;
 - D-wall excavation
 - D-Wall concreting
 - Bulk Excavation
- 3D numerical modelling of soil structure interaction used to predict changes



K₀ variation in Chalk Rock during construction

Geotechnical Design and Analysis



Ground-Shaft-Tunnel interaction analysis enabled us to:

- Understand the clear load path and the arching/relaxation effects of the surrounding ground
- Determine forces on the structural elements at different construction stages
- Optimise diaphragm wall thickness & collar structure.

Construction Methods Planning



Construction



Chalfont St Giles September 2022



Chalfont St Peter Ground Treatment



Chalfont St Peter Collar Installation

Actual v Predicted

Hoop forces are key to shaft stability

Geotechnical design set instrumentation trigger values

- Stresses
- Strain

Monitoring demonstrated:

- compliance with trigger values
- also validated the design parameters used

$$K_{0-3} = \frac{\sigma'_h}{\sigma'_v} = 1.05 \text{ affecting the shafts during excavation}$$

- provides data for research & development



Thank you

